# WIN-SABRE

### Tutorial for ASD & LRFD (Cantilever)

Windows-Based Computer Analysis of 3-D Sign Bridge



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#### Step 2: Input General Program Options (Detailed level is needed for Postprocessor)





# Step 3: Select Configuration Type

	Yield Stresses	Definition of Sections	VAMS
guration <b>Eler</b>	nent Definition	Dimensions	Cross Sections
CANTILEVER	O SPAN	O B	UTTERFLY
			I /
SPAN WITH 1 CANTILEVER		O DOUBLE S	PAN



**Step 5: Predefine Cross Section Numbers** (see the screen for Definition of Sections) and assign them to Posts and Chords. (In this example, Section 1 for post and 2 for chords) <u>Edit Input Screen Go To Input G</u>raph 🕹 🔂 N? 🖂 🕅 🖬 🖬 😂 🖬 🖻 👗 🛍 🖻 🛶 Signs Bracing **Yield Stresses** on of Sections VAMS Configuration **Element Definition** imensions **Cross Sections** Cantilever **DATA TYPE: 33000** CT =col top CB =col bottom BLT =beam left top BLB =beam left bottom BC =beam center CT BLT BRT BRT =beam right top 1 2 2 BRB =beam right bottom LCT =left col top LCB =left col bottom 2 BLB CB 1 RSITY OF 

#### Step 6: Input Dimensions 🚆 e:\temp\sspc1.dat - [Structure Generation] 🙀 File Edit Input Screen Go Io Input Graphic Help. D 🗃 🖬 🐰 🛍 🛈 🛶 🖓 🎓 🐶 🔜 🛛 Mesh Signs **Yield Stresses Definition of Se** VAMS Bracing **Cross Sections** Configuration **Element Definition** Dimensions Cantileve DATA TYPE: 34000 BEAM LENGTH : 52.166 LOW CHORD BEAM ELEV.: 20.729 **BEAM DEPTH** : 6.0 BEAM WIDTH : 6.0 : CONNECTION LENGTH 2.0 **TOWER WIDTH**: LAST BRACE : FIRST BRACE: TOP ELEV. : 26.729 BOT. ELEV. : 0.0 LAND

#### Step 7: Input Bracing Patterns and Section Numbers (In this example, no perpendicular, only diagonal bracing.)



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	Element Definition	Dimensio	Cross Sections
Bracing	Yield Stresses	Definition of S	
DATA TYPE: 39000 MEMBER TYPE	TOWERS	BEAMS	
MAIN MEMBERS	46.0 ksi(MPa)	46.0 ksi(MPa)	
PERPENDICULAR BRACING	36.0 ksi(MPa)	36.0 ksi(MPa)	
DIAGONAL BRACING	36.0 ksi(MPa)	<b>36.0</b> ksi(MPa)	



Step 9: Define Sections used on the Cross Section screen (This example assigns 1 for the post, 2 for the chords, 4 for the bracing and 6 for the VAMs)

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	C	onfigura	tion		Ele	ment De	fin	Dimensions					Cross S	ections
	Pr:	Signs		γĒ	Viek		7 /	Definition of Continue					VAMS	
TA TYPE: 04012									Definition of Sections     VAM5     Section Lookup				p	
_		Std. Se	ect.		Tubula	r Shapes	\$			G	ieneral Se	ctions		
Sec No	ID	DTH inch (mm)	WT/FT (Lb./ft)	ID	OUT D inch (mm)	Tw inch (mm)	Kt	ID	WT/FT Kip/ft (KN/m)	S1 inch (mm)	S2 inch (mm)	S3 inch (mm)	S4 inch (mm)	S5 inch (mm)
11				2	34.0	0.375	1.0							
2				2	6.625	0.280	1.0							
3				2	6.625	0.280	1.0							
4				2	2.375	0.154	1.0							
5		-	0	2	2.375	0.154	1.0		000	2.040	E 000	0.015		0.170
<u>р</u> 2	w	ь	9	000				9	.009	3.940	5.900	0.215		0.170
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Step 10: Define Vertical Attachment Members and their relationship to the Sign and Walkway (This example has 11 VAMs where 7-11 support Sign #1 and Walkway #1. Section 6 for all the VAMs)

Dimensions **Cross Sections** Configuration Signs Bracing Definition of Sections VAMS Stresses DATA TYPE: 07012 Attached Sign Units VAM ID Top VAM Coords. Supporting Members Walkway Units х Y z Length No Sect. No. No. No. No. No. feet feet feet feet No. No. No. No. (m) (m) (m) (m) 3.25 27.0 1.1 6.813 21 1 6 7 2 6 7.417 27.0 1.1 6.813 8 22 3 6 13.25 27.0 6.813 10 24 1.1 4 6 17.417 27.0 1.1 6.813 11 25 5 6 23.25 27.0 6.813 12 26 1.1 6 6 27.0 6.813 14 28 29.25 1.1 7 6 34.917 31.729 1.1 11.542 16 30 1 1 8 6 11.542 17 31 1 38.917 31.729 1.1 1 9 6 42.917 31.729 11.542 32 1.1 18 1 1 10 6 46.917 31.729 1.1 11.542 19 33 1 1 11.542 20 11 6 50.917 31.729 1.1 34 1 1 12 13 14 15 16 17 18 19 Step 10A: Supporting Members are figured out by the Mesh. No input is needed 💖 MARYLAND

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ElemEditorInput Screen

	Braci	ng		Yield	l Stresses	1	Defir	nition of Se	ections	VAMS
	Configura	tion		Element	Definition		D	imensions		Cross Sections
A TY	Signs	3								
		a Dimension	s			Lo	wer Left Co	oord.	]	
iign No.	Width feet (m)	Height feet (m)	Thick. inch (mm)	Slope in/ft (mm/m)	Density k/cf (Kg/m^3)	X feet (m)	Y feet (m)	Z feet (m)		
	17.719	9.0	0.35		0.175	34.354	22.729	1.15		
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4										
5 6										
7 8										
9										
0									]	
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#### No Step: Parameters are generated by Mesh, unless override is needed



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#### No Step: Joint Loads are generated by Mesh, unless additional Join Load is needed

<b>2</b> 1				- J 4	N2 11	Mesh				
					<u></u>	псын			Υ	
		Lonr	nections	,	, <u> </u>	Heig	ht Coeff. *		Hinges	
		Param	eters			Joint L	.oads	L		Walkways
DA	ΓΑ ΤΥ	'PE : 10	012							
					Forces			Moments		
	No	Joint No.	Desc.	X kip(KN)	Y kip(KN)	Z kip(KN)	X-X k-ft (KN-m)	Y-Y k-ft (KN-m)	Z-Z k-ft (KN-m)	
I	1									
	2									_
	3									_
	4									_
	0									-
	7									-
	8									-
	9									-
	10									-
	11									-
	12									
	13									
	14									
	15									
	16									
	17									
	18									
	19									







#### No Step: Height Coefficients are generated by Mesh, unless override is needed





# No Step: Hinges, if exist, are generated by the program, unless overridden

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	Mash					
	THESH	loistloosda		$\gamma \rightarrow \gamma$	No Statements	<u></u>
Connections	He	ight Coeff	Ý		Hinges	<u></u>
DATA TYPE : 40000	LEFT B	EAM END	RIGHT E	EAM END		
	Y-Y	Z-Z	Y-Y	Z-Z		
	(	) or 1)	(0	or 1)		
монотиве		1		1		
PLANE TRUSS						
TRICHORD TRUSS ON 1 POST						
BOX TRUSS ON 1 POST						
TRICHORD TRUSS ON 2 POSTS	1	1	1	1		
BOX TRUSS ON 2 POSTS	1	1	1	1		
						-



#### Step 12A: Once done, click Mesh button and then Input Graphic on the Menu Bar

		Cor	nnections					Heigh	t Coeff.		Hinges		
					_	Joint Loads						Walkway	
	UAI Wal	A IYI kwai	YE: 08012	d Ends		ad T	une -	Uniform	Loading.	Wind	Areas	1	
		No	Left feet(m)	Right feet(m)	DL	ICE	LL	LOAD klf (KN/m)	Z Coord. feet(m)	Area ft^2/ft (m^2/m)	Y Coord. feet(m)		
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Step 14: Save the Input File, Exit from Input Utility and click Analysis

<pre>Prove Analyse Dubud Graphic PolyPocessing Ent Heb Poly Analyse Dubud Graphic PolyPocessing Ent Heb Prace soleci files:</pre>	SABRE Program		
Image: Control of the contro	Exit Input Analysis Output Graphics Post Prod	cessing <u>P</u> rint <u>H</u> elp	
Freede SADE			
Place select file: Input File e:\temp\sspc1.dat DegarFile e:\temp\sspc1.out		Execute SABRE	
Insuffie e:\temy\sspc1.dat DeputFie e:\temy\sspc1.out		Please select files:	
e:\temy\sspc1.at Duput File e:\temy\sspc1.out		Input File	
Durger File e: \temp\sspcl.out		e:\temp\sspc1.dat	
e:\temp\sspc1.out		Output File	
		e:\temp\sspc1.out	
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Step 15: Exit from Analysis, click Output Graphics and select one item under ActDef for analysis status

Graphics for E:\temp\sspc1.out					
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Woerner Wire Works Test					
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			$\mathbb{V}$ $\mathbb{V}$ $\mathbb{V}$ $\mathbb{V}$	a vi vi v	
			Î Î		
	List of Del	flections Tables in E:	temp\sspc1.out	×	
	Group	Joint Deformation	s-DL	·	
	Group II Group II	Joint Deformation	s - DL+W Combo. 1 s - DL+W Combo. 2	in +2 lin +Z	
	Group II	Joint Deformation	s - DL+W Combo. 1	in -Z	
	Group II Group II	Joint Deformation	s - DL+W Combo. 2 >s - DL+L+1/2W Con	? in -Z	
	Group II	I Joint Deformatio	is - DL+I+1/2W Con	nbo. 2 in +Z	
	Group II	I Joint Deformation	is - DL+I+1/2W Con	nbo. 1 in -Z	
	Maximur	n Joint Deformation	15 - DE+1+17214 CON NS	100. Z III -Z	
					VERSIT RVI A

Step 16: Exit from Output Graphics, select Post Process, Base Plate Design and then click Import for the analysis results

Post Processing - E:\t	emp\sspc1.out			
Splice Plate Desig	in Parameters	Base Plate Design Parameters	Base Plate Fatigue Check	
Ext	Calculate Import			
ENG/SI UNIT	0 0 - English 💌			
YIELD STRESSES		COLUMN PARAMETERS		
BOLT	55.00 ksi(MPa)	OUTSIDE DIAMETER 34.	in(mm)	
BASE PLATE	36.00 ksi(MPa)	WALL THICKNESS .37	5 in(mm)	
COLUMN	55.00 ksi(MPa)	CROSS-SECTION SHAPE 2	2 - Round cross section	
BASE FORCES		BASE MOMENTS		
X DIR.	1.961 kips(KN)	X-X AXIS 236	.429 k-ft[KN-m]	
Y DIR.	10.94 kips(KN)	Y-Y AXIS	7.508 k-ft(KN-m)	
Z DIR.	9.591 kips(KN)	Z-Z AXIS	5.127 k-ft(KN-m)	
ALLOWABLE WELD	STRESS 12.40 ksi(M	Pa) BASE PLATE SHAPE 2	2 - Round cross section	
GROUP LOAD NO.	2	DES. NO OF BOLTS		8
		Base Pla	ate Design Results	
		NO. OF B BOLT DIA	OLTS =8 AMETEB =1.5 in	
		BOLT AR	EA (EACH) =1.767 in.^2 ENT LENGTH =4.9 ft	
			JDOAT LENGTH - 221 in	
		WELD LE	G LENGTH =.313 in.	
			HAPE = Round	
	The tele the entir	PLATE 0 PLATE S	IDE LENGTH =18.6 in.	
Step 16A: F	-inish the Ir		HILKNESS =.33 IN.	
click Calcul	ation to she			
			àraph Print	JNIVERSITY OF
the design				J MARYLAND

Step 17: Click Graph on the Calculation popup screen to show the design



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#### Step 18: Exit from Base Plate Design and Click the Tab for Base Plate Fatigue Check

Splice Plate Design Parameters	Base Plate Design Parameters	Base Plate Fatigue Check
Exit Calculate Import	Print	
ENG/SI UNIT 0 0 - English 💌		
BASE MOMENT RANGE	COLUMN PARAMETERS	5
X-X AXIS 35.15 (k-ft or KN-m)	OUTSIDE DIAMETER	34. (in or mm)
Z-Z AXIS 143.8 (k-ft or KN-m)	WALL THICKNESS	0.38 (in or mm)
	CROSS SECTION SHAF	PE 2 2 - Round cross section
BASE PLATE PARAMETERS	STIFFENER PARAMETE	ERS
SHAPE 2 - Round cross section	HEIGHT	(in or mm)
BOLT DIAMETER (in or m	m) WIDTH	(in or mm)
BOLT THREAD PITCH (in or m	m) THICKNESS	(in or mm)
FARTHEST BOLT DISTANCE	m) TOTAL NUMBER	
NUMBER OF BOLT		
Step 18A: Click Impo	ort, finish	
all the input and then	click	

#### Step 19: Exit from Post Process. Click Print and then Open File

Re:\temp\sspc1		1998) 1998
Open File View/Print File Vie	w Tables Print Tables Exit	
File Name: SSPC1.OUT sspc1.out Sspc1a.out Sspc1b.out sspc1c.out	OK     Image:	



# Step 20: View or Print the whole File or Table by Table

Dese File Manufick File Manuficker Dist Tables Freit	
1.0 : INPUT VERIFICATION	
1.1 : DEFINITION OF JOINTS	
1.2 : DEFINITION OF SECTIONS	
1.3 : DEFINITION OF MEMBERS	
1.4 : DEFINITION OF VERTICAL ATTACHMENT MEMBERS	
1.5 : DEFINITION OF WALKWAYS AND CONDUITS	
1.6 : DEFINITION OF SIGNS	
TABLE 1.U : INPUT VERIFICATION	
DEFINITION OF SYSTEM DATA	
OUTPUT DESIGN DESIGN DESIGN STRU. NO. OF NO. OF MATERIAL AL	
LEVEL CODE YEAR OPTION TYPE POSTS CORDS UNIT TYPE E MODULUS ID	
DESIGN PARAMETERS	
WIND MEAN VEL. VER. SPEED IMPORT MEAN REC GUST ICE ICE DEAD VIET N.W. CUST T. CUST TANCE INTERVAL FAC LOADS LOAD LOAD	
(MPH) (MPH) (MPH) FACT. (YEARS) (%) (PSF) OPTN FAC.	
80.00 .0 .0 .00 50 30.00 3.000 0 1.00	

# **AASHTO LTS-6 & AASHTO LTS-LRFD**

Updated SABRE includes following improvements:

AASHTO LST-6 & AASHTO LTS-LRFD Fatigue Design

 Design parameters based on fatigue importance category
 Cantilever and non-cantilever structures

### 2. AASHTO LTS-LRFD Design

- a. Determination of wind speed and wind pressure
- b. Example of wind speed and wind pressure
- c. Wind strength design consideration



# **Fatigue Design Parameters**

Fatigue Importance Category		Galloping Natural Wind Gusts		Truck-Induced Gusts	
red	I	<b>Sign</b> Traffic Signal	<b>1.0</b> 1.0	<b>1.0</b> 1.0	<b>1.0</b> 1.0
ntileve	Ш	Sign Traffic Signal	0.70 <mark>0.65</mark>	0.85 <mark>0.80</mark>	0.90 <mark>0.85</mark>
Car	ш	Sign Traffic Signal	0.40 0.30	0.70 0.55	0.80 0.70
red	I	<b>Sign</b> Traffic Signal	X X	<b>1.0</b> 1.0	<b>1.0</b> 1.0
Non- ntileve	II	<b>Sign</b> Traffic Signal	x x	<b>0.85</b> 0.80	<b>0.90</b> 0.85
Car	Ш	Sign Traffic Signal	x x	0.70 0.55	0.80 0.70

- Cat. I without "mitigation devices"; roadways with a speed limit in excess of 60 km/h (35 mph) and average daily traffic (ADT) exceeding 10,000 or average daily truck traffic (ADTT) exceeding 1000
- Cat. III speed limits 60km/h (35 mph) or less
- Cat. II not "explicitly" meeting I or III; (NCHRP 469 Act. 3.2.1.4: include any store with mitigation devices that would otherwise meet the Category I criteria.)

# 1. Introduction : Fatigue Design Loads - Galloping





### 1. Introduction : Fatigue Design Loads – Natural Wind & Truck-Induced Gust







# **Fatigue Details**

#### SABRE Fatigue Design Input

Source: NJDOT report "Fatigue Study on Structural Supports for Luminaries, Traffic Signals, Highway Signs", Chapter 8 example 1

Parameters		Additional Joint Loads	Walkways
DATA TYPE: 01042			
VIND VELOCITY	80.0	(mph or m/s)	
EAN REGULAR INTERVAL	50	(years)	
SUST FACTOR	1.14	Regular Method - 1.14 (4th or 5t	ed.)
CE LOADS	3.0	(psf or KPa) ICE LOAD OPTIO	NS 0 0- One Side 🗸
RUSS BRACING OPTIONS	0 0- Mome	nt Bracing (default) 📃 💌	
). L. DETAIL FACTOR	1.0		
VIND IMPORTANCE FACTOR	1.0	(default = 1.0; see AASHTO Tab	le 3-2)
For Fatigue Design Only			
ZEARLY MEAN VELOCITY	11.2 (de	fault = 11.2 mph or 5 m/s)	
/EHICLE SPEED FOR TRUCK-INDUCED GUST	65. (de	fault = 65 mph or 30 m/s)	
ATIQUE IMPORTANCE FACT	OR OPTIONS		<b>•</b>
GALLOPING (default = 1.0)	NATURAL WIN	ID (default = 1.0) TRUCK - I	NDUCED GUST (default = 1.0)

# **SABRE Fatigue Verification**

# Sabre calculation, NJDOT report and STAAD fatigue calculation comparison

Example I	(Fatigue II)	Sabre	Report	STAAD
	Gallop	7.056	7.056	7.056
	Natural wind total	3.761	3.2551*	3.237*
	sign	2.534	2.545	2.544
loint load (kins)	chord	0.703	0.17	0.17
	column	0.525	0.5401	0.522
	Truck.W	0.408	0.271	0.271
	TW sign	0.134	0.134	0.134
	TW chord	0.274	0.137**	0.137**
	Gallop	169.9	169	169.3
Moment (K-ft)	Natural.W	63.6	57.65	61.1
	Truck.W	13.92	8.87	9.21



## Fatigue Check Example using Spreadsheet

# Fatigue check using the spreadsheet example

- The sabre output file element #1 represent the base plate. The output list moments for both ends of element. Please select the higher moment from the table.
- The sabre file is in kip-ft unit, the spreadsheet is in kip-in. In this case, the moment should be, 6.2\*12=74.4 kip-in.

+	•		•	► diam. co → dia	olumn m. bolt circle diam. base	Anc	hor rod stres culation for N rods	S		
$Z_3$	$\langle \circ \rangle$	0	Ľ	$\geq$						
	$\gamma$	Г	_× ۲	$\left  \right\rangle$						
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		_		F 13						
				- 13						
Dia d <sub>ar</sub> =		2.	<mark>5</mark> in	Red ink	cells are for	input				
Dia d <sub>ar</sub> = Thread series=		2.	<mark>5</mark> in 4 unc	Red ink	cells are for	input				
Dia d <sub>ar</sub> = Thread series= Crcle dia d <sub>are</sub> =		2.	<mark>5</mark> in 4 unc 2 in	Red ink	cells are for	input				
Dia d <sub>ar</sub> = Thread series= Crcle dia d <sub>arc</sub> = M <sub>Z TG base</sub> =		2. 3 74.	5 in 4 unc 2 in 4 kip-in	Red ink	cells are for	input nent fr	om Sabre.	k-in		
Dia d <sub>ar</sub> = Thread series= Crcle dia d <sub>arc</sub> = M <sub>Z,TG,base</sub> = Number of ancho	r rods =	2. 3 74.	5 in 4 unc 2 in 4 kip-in 6	Red ink (min. 4 t	cells are for mol	input nent fr	om Sabre,	k-in		
Dia d <sub>ar</sub> = Thread series= Crcle dia d <sub>arc</sub> = M <sub>Z,TG,base</sub> = Number of ancho	r rods =	2. 3 74.	5 in 4 unc 2 in 4 kip-in 6	Red ink (min. 4 t	cells are for mol	nput nent fr	om Sabre,	k-in		
Dia d <sub>ar</sub> = Thread series= Crcle dia d <sub>arc</sub> = M <sub>Z,TG,base</sub> = Number of ancho Thread pitch =	r rods =	2. 3 74. 0.24357	5 in 4 unc 2 in 4 kip-in 6 5 in	Red ink (min. 4 b	molts)	nput nent fr	om Sabre,	k-in		
Dia d <sub>ar</sub> = Thread series= Crcle dia d <sub>arc</sub> = M <sub>Z,TG,base</sub> = Number of ancho Thread pitch =	r rods =	2. 3 74. 0.24357	5 in 4 unc 2 in 4 kip-in 6 5 in	Red ink (min. 4 b	cells are for mon	nput nent fr	om Sabre,	k-in		
Dia $d_{ar} =$ Thread series= Crcle dia $d_{arc} =$ M <sub>Z,TG,base</sub> = Number of ancho Thread pitch = A <sub>T</sub> = $\pi/4(d_{ar}-0.9743)$	r rods = 3/n) <sup>2</sup>	2. 3 74. 0.24357	5 in 4 unc 2 in 4 kip-in 6 5 in	Red ink (min. 4 t	cells are for mon	nput nent fr	om Sabre,	k-in		
Dia $d_{ar}$ = Thread series= Crcle dia $d_{arc}$ = $M_{Z,TG,base}$ = Number of ancho Thread pitch = $A_T = \pi/4(d_{ar} - 0.9743)$ $A_T$ =	r rods = 3/n) <sup>2</sup> 4.00	2. 3 74. 0.24357 in <sup>2</sup>	5 in 4 unc 2 in 4 kip-in 6 5 in	Red ink (min. 4 t	cells are for mon	nent fr	om Sabre,	k-in		
Dia $d_{ar} =$ Thread series= Crcle dia $d_{aro} =$ $M_{Z,TG,base} =$ Number of ancho Thread pitch = $A_T = \pi/4(d_{ar} - 0.9743)$ $A_T =$	r rods = 3/n) <sup>2</sup> 4.00	2. 3 74. 0.24357 in <sup>2</sup>	5 in 4 unc 2 in 4 kip-in 6 5 in	Red ink (min. 4 t	cells are for monolts)	nent fr	om Sabre,	k-in		
Dia $d_{ar} =$ Thread series= Crcle dia $d_{aro} =$ $M_{Z,TG,base} =$ Number of ancho Thread pitch = $A_T = \pi/4(d_{ar} - 0.9743)$ $A_T =$ $I_{ar} = \Sigma A_T Z^2$	r rods = 3/n) <sup>2</sup> 4.00	2. 3 74. 0.24357 in <sup>2</sup>	5 in 4 unc 2 in 4 kip-in 6 5 in	Red ink (min. 4 t	cells are for mol polts)	nent fr	om Sabre,	k-in		
Dia $d_{ar} =$ Thread series= Crcle dia $d_{arc} =$ $M_{Z,TG,base} =$ Number of ancho Thread pitch = $A_T = \pi/4(d_{ar} - 0.9743$ $A_T =$ $I_{ar} = \Sigma A_T z^2$ $I_{ar} =$	r rods = 3/n) <sup>2</sup> 4.00 3112.33	2. 3 74. 0.24357 in <sup>2</sup>	5 in 4 unc 2 in 4 kip-in 6 5 in	Red ink (min. 4 t	cells are for mol polts)	nent fr	om Sabre,	k-in		
Dia $d_{ar} =$ Thread series= Crcle dia $d_{arc} =$ $M_{Z,TG,base} =$ Number of ancho Thread pitch = $A_T = \pi/4(d_{ar} - 0.9743)$ $A_T =$ $I_{ar} = \sum A_T z^2$ $I_{ar} =$ Stress range	r rods = 3/n) <sup>2</sup> 4.00 3112.33	2. 3 74. 0.24357 in <sup>2</sup>	5 in 2 in 4 kip-in 6 5 in	Red ink (min. 4 t	cells are for mol polts)	nent fr	om Sabre,	k-in		
Dia $d_{ar} =$ Thread series= Crcle dia $d_{arc} =$ $M_{Z,TG,base} =$ Number of ancho Thread pitch = $A_T = \pi/4(d_{ar} - 0.9743)$ $A_T =$ $I_{ar} = \sum A_T z^2$ $I_{ar} =$ Stress range (fip) not MZ TG have	r rods = 3/n) <sup>2</sup> 4.00 3112.33 • x c/lar	2. 3 74. 0.24357 in <sup>2</sup>	5 in 4 unc 2 in 4 kip-in 6 5 in	Red ink (min. 4 t	cells are for mol polts)	nent fr	om Sabre,	k-in		
Dia $d_{ar} =$ Thread series= Crcle dia $d_{arc} =$ $M_{Z,TG,base} =$ Number of ancho Thread pitch = $A_T = \pi/4(d_{ar} - 0.9743)$ $A_T =$ $I_{ar} = \sum A_T Z^2$ $I_{ar} =$ Stress range (fR)rod = MZ,TG,base (fR)rod =	r rods = 3/n) <sup>2</sup> 4.00 3112.33 • x c/l <sub>ar</sub>	2. 3 74. 0.24357 in <sup>2</sup>	5 in 4 unc 2 in 4 kip-in 5 in 5	Red ink (min. 4 t	cells are for mol polts)	nent fr	om Sabre,	k-in		
Dia $d_{ar} =$ Thread series= Crcle dia $d_{arc} =$ $M_{Z,TG,base} =$ Number of ancho Thread pitch = $A_T = \pi/4(d_{ar} - 0.9743)$ $A_T =$ $I_{ar} = \sum A_T Z^2$ $I_{ar} =$ Stress range $(f_R)_{rod} = MZ, TG, base$	r rods = 3/n) <sup>2</sup> 4.00 3112.33 x c/l <sub>ar</sub> 0.38	2. 3 74. 0.24357 in <sup>2</sup> in <sup>4</sup>	5 in 4 unc 2 in 4 kip-in 5 in 5 in Category	Red ink (min. 4 t	cells are for mol polts)	nent fr	om Sabre,	k-in		

### Wind Speed/Pressure

Wind loads based on 2013 ASD (STD-LTS) and 2015 LRFD are shown below: a) 2013 wind pressure

#### Pz=0.00256K<sub>z</sub>\*G\*V<sup>2</sup>\*I<sub>r</sub>\*C<sub>d</sub>

b) 2015 LRFD wind pressure

#### Pz=0.00256K<sub>z</sub>\*K<sub>d</sub>\*G\*V<sup>2</sup>\*C<sub>d</sub>

AASHTO LRFD-LTS Table 3.8-1 – Mean Recurrence Interval

	Risk Category					
Traffic Volume	Typical	High	Low			
ADT ≤ 100	300	1700	300			
100 < ADT ≤ 1000	700	1700	300			
1000 < ADT ≤ 10000	700	1700	300			
ADT > 10000	1700	1700	300			
Typical: Eailura could groep trovoly	0)/					

Typical: Failure could cross travelway

High: Support failure could stop a lifeline travelway

Low: Support failure could not cross travelway

Roadside sign supports: use 10-yr MRI, see Figure 3.8-4

### **Example of Maryland Wind Speed/Pressure**



## **Example of Wind Speed/Pressure**

Assumption:

 $K_z = 0.87$  for 2013 and 084 for the 2015 LRFD Specifications

 $K_d = 0.85$  (signal and sign support structures) for the 2015 LRFD Specifications only

G = 1.14 for both

 $C_d = 1.20$  for both

 $I_r = 1.00$  for the 2013 Specifications only

Case 1	2013	2015 LRFD	2015 LRFD	2015 LRFD
Wind speed (V)	100mph	100mph	110mph	120mph
Pz	30.47	25.01	30.26	36.01

- For LTS-6 (2013) still use wind speed 100 mph statewide, which is equivalent for 110 mph for LTS-LRFD (2015)
- For LTS-LRFD (2015) may consider using wind speed 120 mph statewide (? To be determined)



## Wind Strength Design Consideration

• LTS-6: Only basic load (BL) on one arm plane is considered

Load Case	Normal	Transverse
	component	component
1	1.0 BL	0.2 BL
2	0.6 BL	0.3 BL

 LTS-LRFD: Two basic load are considered (BLn) on one arm plane/(BLt) on the arm plane spaced at 90 degree

Load Case	Normal	Transverse
	component	component
1	1.0 BLn	0
2	0	1.0 BLt
3	0.75 BLn	0.75BLt



## **SABRE Input & Analysis Module for LRFD**

Parameters	Additional Joint Loads	Walkways					
DATA TYPE: 01042			C	Soo tha	- rod_ir	hk	
WIND VELOCITY	120. (mph or m/s)	(mph or m/s) (SERVICE I, LRFI	D only)			ш	
MEAN REGULAR INTERVAL	50 (years)		b	lock fo	or the o	only	У
GUST FACTOR	1.14 Regular Method - 1.14 (4th or 5th	ed.) 💌	ir	nnut ch	anao	of	
ICE LOADS	3.0 (psf or KPa) ICE LOAD OPTIONS	0 0- One Side 👻		iput ci	lange	U	
TRUSS BRACING OPTIONS	0- Moment Bracing (default)			.RFD			
D. L. DETAIL FACTOR	1.0						
ASD: WIND IMPORTANCE FA	CTOR or (default = 1.0; see AA	SHTO Table 3-2)					
LRFD: DIRECTIONALITY FAC	TOR, Kd post default = 0.95, 4 see AASHTO LRFD T (post) (others)	others = 0.85, able 3.8.5-1)					
<u>For Fatigue Design Only</u>							
YEARLY MEAN VELOCITY For natural wind gust	(default = 11.2 mph or 5 m/s)						
VEHICLE SPEED FOR TRUCK-INDUCED GUST	(default = 65 mph or 30 m/s)						
FATIGUE IMPORTANCE FACT	OR OPTIONS	<b>•</b>					
GALLOPING (default = 1.0)	NATURAL WIND (default = 1.0) TRUCK - IND	UCED GUST (default = 1.0)					
Overall Effective Length H	(Table 7.4.1 of the User's Manual)						
CASE 1: VERTICAL (POLE TY	PE) (default = 2.0)	SABRE Pro	gram	- Frank			
CASE 2: VERTICAL (TRUSS T	YPE) (default = 1.2)	Exit Input	Analysis Outpu	it Graphics Po	ost Processing	Print	Help
CASE 3: HORIZONTAL (POLE	AND TRUSS) (default = 0.65)	×	SABRE - LR	FD			
			SABRE - AA	SHTO 5th - 6th	Edition		
40			SABRE - AA	SHTO 4th Editio	on		
40			SABRE - AA	SHTO 3rd Editio	on		

# **SABRE Load Combinations for LRFD**

A. Strength Limit State

- Group 1 1.25DL + 1.6LL (T8.1, check for T10.1 & T13.1)
- B. Extreme Limit State
  - Group 2 1.1DC+W (Comb 1 +Z) (T8.2, check for T10.2, T13.2)
  - Group 2 1.1DC+W (Comb 2 +Z) (T8.3, check for T10.3, T13.3)
  - Group 2 1.1DC+W (Comb 3 +Z) (T8.4, check for T10.4, T13.4)
  - Group 2 1.1DC+W (Comb 1 -Z) (T8.5, check for T10.5, T13.5)
  - Group 2 1.1DC+W (Comb 2 -Z) (T8.6, check for T10.6, T13.6)
  - Group 2 1.1DC+W (Comb 3 -Z) (T8.7, check for T10.7, T13.7)
  - Group 3 0.9DC+W (Comb 1 +Z) (T8.8, check for T10.8, T13.8)
  - Group 3 0.9DC+W (Comb 2 +Z) (T8.9, check for T10.9, T13.9)
  - Group 3 0.9DC+W (Comb 3 +Z) (T8.10, check for T10.10, T13.10)
  - Group 3 0.9DC+W (Comb 1 -Z) (T8.11, check for T10.11, T13.11)
  - Group 3 0.9DC+W (Comb 2 -Z) (T8.12, check for T10.12, T13.12)
  - Group 3 0.9DC+W (Comb 3 -Z) (T8.13, check for T10.13, T13.13)

#### C. LRFD Strength/Extreme Limit State Combination Checks

- Tower and Truss Member Capacities (T11.2 & T12.2)
- Tower and Truss Member Maximum Combined Force Ratios (CSR) (T11.4 & T12.4)

## **SABRE Load Combinations for LRFD**

#### D. Service I Limit State

- Group 4 1.0DC+ W<sub>SE</sub> (Comb 1 +Z) (T8.14, check for T9.14)
- Group 4 1.0DC+ W<sub>SE</sub> (Comb 2 +Z) (T8.15, check for T9.15)
- Group 4 1.0DC+ W<sub>SE</sub> (Comb 3 +Z) (T8.16, check for T9.16)
- Group 4 1.0DC+ W<sub>SE</sub> (Comb 1 -Z) (T8.17, check for T9.17)
- Group 4 1.0DC+ W<sub>SE</sub> (Comb 2 -Z) (T8.18, check for T9.18)
- Group 4 1.0DC+ W<sub>SE</sub> (Comb 3 -Z) (T8.19, check for T9.19)

#### E. LRFD Service Limit State Deflection Checks

Maximum Joint Deflection tables (T9.10)

#### F. LRFD Fatigue Limit State Checks

- Group 5 Galloping (T19.1, T9.11, T10.11, check for T20.1)
- Group 5 Natural Wind Gust (T19.2, T9.12, T10.12, check for T20.2)
- Group 5 Truck Gust (T19.3, T9.13, T10.13, check for T20.3)

